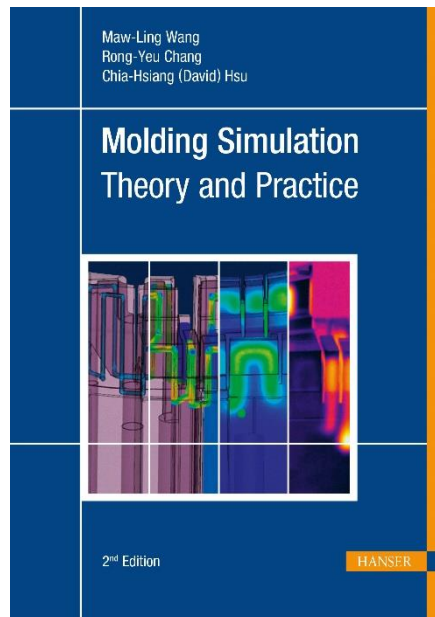


# HANSER



## Sample Pages

### **Molding Simulation: Theory and Practice**

Maw-Ling Wang, Rong-Yeu Chang and Chia-Hsiang  
(David) Hsu

ISBN (Book): 978-1-56990-884-6

ISBN (E-Book): 978-1-56990-885-3

**For further information and order see**

[www.hanserpublications.com](http://www.hanserpublications.com) (in the Americas)

[www.hanser-fachbuch.de](http://www.hanser-fachbuch.de) (outside the Americas)

© Carl Hanser Verlag, München

# Acknowledgments

We would like to thank and acknowledge Beaumont Technologies, Inc. for the flow imbalance case in Section 7.1.4 and Section 7.2.1, OPM Laboratory Co., Ltd. for the conventional and conformal cooling design cases in Section 8.2.1, Associate Prof. Chao-Tsai Huang for the coupling effects between flow and fibers study of ASTM D638 standard test pieces in Section 10.2.3, Ann Tong Industrial Co., Ltd. For the single-gate hot runner system case in Section 11.2.1, Associate Prof. Chao-Tsai Huang for co-injection molding of standard tensile bar test piece in Section 12.2.3, Prof. Shi-Chang Tseng and Prof. Shia-Chung Chen for the gas-assisted injection molding cases in Section 13.2.1 and Section 13.2.3, respectively, Prof. Shih-Jung Liu for the water-assisted injection molding case in Section 13.2.2, Trexel Inc. for the MuCell® case in Section 14.2.1, Proplast, Inc. for the U-shape model of micro-cellular injection molding in Section 14.2.2, Prof. Shyh-Shin Hwang for the chemical foaming injection molding case in Section 14.2.3, Prof. Shun-Tian Lin for the metal injection molding case in Section 15.2.1, Atech Composites Co., Ltd. for resin transfer molding cases in Section 16.3.3 and Section 16.3.5, Associate Prof. Yuan Yao for the resin transfer molding case in Section 16.3.4, and Amkor Technology Korea Inc. for the IC packaging cases in Section 17.2.1 and Section 17.2.2. These practical cases are quite valuable and helpful to illustrate how to co-develop innovative molding technologies and solve molding issues with the CAE tool.

We would also like to thank the following for their contributions: Dr. Che-Ping (Barton) Lin on Chapter 1, Dr. Chen-Chieh (Jye) Wang and Dr. Chih-Wei (Joe) Wang on Chapter 2, Tsai-Hsin (Sam) Hsieh, Tsai-Heng (Paul) Tsai, Dr. Ying-Mei (May) Tsai, Dr. Yao-Chen (Cloud) Tsai, and Yao-Wei (Willie) Chuang on Chapter 3, Tsai-Hsin (Sam) Hsieh, Wen-Bing (Webin) Liu, Dr. Ying-Mei (May) Tsai, and Dr. Chuan-Wei (Arvid) Chang on Chapter 4, Hsien-Sen (Ethan) Chiu and Dr. Ying-Mei (May) Tsai on Chapter 5, Yu-Chih (Goran) Liu, Wen-Bing (Webin) Liu, and Wen-Hsin (Debbie) Weng on Chapter 6, Dr. Che-Ping (Barton) Lin, Dr. Sung-Wei (Franz) Huang, Dr. Yao-Chen (Cloud) Tsai, and Yao-Wei (Willie) Chuang on Chapter 7, Dr. Chih-Wei (Joe) Wang, Dr. Sung-Wei (Franz) Huang, and Hung-Chou (Kent) Wang on Chapter 8, Dr. Shih-Po (Tober) Sun and Wen-Hsin (Debbie) Weng on Chapter 9, Dr. Huan-Chang (Ivor) Tseng on Chapter 10 and Chapter 15, Tsai-Hsin (Sam) Hsieh on Chap-

ter 11, Dr. Chih-Chung (Jim) Hsu and Yu-Sheng (Tim) Chou on Chapter 12 and Chapter 13, Yuan-Jung (Dan) Chang, Li-Yang (Robert) Chang and Chih-Wei (Joe) Wang on Chapter 14, Hsun (Fred) Yang on Chapter 16, and Chih-Chung (Jim) Hsu, Chia-Peng (Victor) Sun, Chen-An (Jennan) Wang, and Yu-En (Joseph) Liang on Chapter 17. They dedicated their wisdom and skills, and a great deal of time, to complete this wonderful book.

Moreover, a very special thanks to Chia-Lin (Carol) Li for redrawing figures, Pao-Hui (Ryan) Wan for his assistive editing, and Dr. Ying-Mei (May) Tsai and Dr. Che-Ping (Barton) Lin for their executive editing.

# Preface

Injection molding techniques have been developed over decades and well-applied in automotive, 3C (Computer, Communication, and Consumer electronics), optics, medical products, and in daily necessities, among other areas. Due to this long-term development and widely ranging applications, the individual molding criteria have been specialized in several industries to fit various product specifications and innovative materials.

The increasing requirements and diversity of plastic products demand a shorter time to market. However, much time can be spent in developing the procedures for some products, from concept generation, design drawing, mold tooling and assembling, and trial-molding through to mass production. “How can the procedures be shortened using CAE (Computer Aided Engineering) tools?” then becomes a key question for industry. The idea is to predict potential molding problems and defects by CAE during the design stage, modify the design according to these results, and then re-analyze until the best design is obtained. This book is written to provide practical and user-friendly guidance in this area. Since the 1970s, virtual trial moldings have been implemented by computer using injection molding simulation CAE tools to check whether the molding parameters are good enough for manufacture. These parameters are part design, gate design, runner layout, cooling layout, molding materials, process conditions, and so on. From CAE, the optimized parameters can be estimated efficiently and provided as the initial-guess settings for the real molding to cost down in time, manpower, material, and energy. To summarize, CAE is a decades-proven design-verification tool for real applications of the injection molding process.

In addition to conventional injection molding, there are many innovative molding processes that have appeared. Molding issues become more challenging and complicated with innovations in processes and materials, which can lead to a longer time and higher costs in conditions optimization. In this 2<sup>nd</sup> edition, the material measurement data are elaborated in Chapter 2 for deeper understanding in polymer processing property effects, including the viscosity comparison between different types or grades of polymer; measurement of viscoelasticity and method to



obtain the master curve; data interpretation of PVT, thermal conductivity, and dynamic modulus of solid-like viscoelastic; and comparison of curing kinetics and reactive viscosity between epoxy molding compounds (EMC). The new concept of connecting Smart Design and Smart Manufacturing is conveyed in Section 4.6 with the methods of Machine Characterization, combination of CAE and injection machine on site, and a practice case.

For further understanding the product quality affected by processing, the flow-fiber coupling model is expressed in Section 10.1.2 to show the flow-induced fiber orientation effect; iARD-RPR models applied with GNF-decoupling and IISO coupling are compared in Section 10.2.2; a study on the tensile strength of test pieces with different gating systems is demonstrated in Section 10.2.3; a microcellular injection part is molded and the sink marks, warpage, and micro characteristics of cell size and cell density are validated by CAE in Section 14.2.2; PU reactive foaming is also addressed in Section 14.2.4 with the material characterization method and a practice case; the experiment with a professional instrument of EASYPERM is illustrated in Section 16.2.3 to obtain the more accurate permeabilities for RTM (Resin Transfer Molding) simulation. And for IC packaging, the warpage of a bi-material component model and a bi-material strip are expounded in Section 17.2.5 and Section 17.2.6, and the effect of dispensing control and creeping behaviors on underfill process is discussed in Section 17.2.7.

From decades of experience in CAE assistance in molding troubleshooting, we have found that processing knowledge is as important as software operation to CAE users. To make a high-quality molded product, the total effects of part design, mold design and manufacture, machine capability, and material properties must all be taken into account and then integrated into the CAE tool to implement design verification and conditions optimization wisely. Each of these definitely involves a deep knowledge, whether in theory and/or empirical formula. When talking about molding issues, plastics rheology and the designs of part and mold are especially the key criteria since their interactions will dominate the material property variations inside the mold.

At Moldex3D, as worldwide leaders in molding simulation software, we are not just continuously enhancing CAE capability but also intend to help industry people improve their molding-related abilities. The importance of training and instruction has become strongly apparent to us. As a result, this book consists of plastics molding theory, practical applications, and case studies intended to elaborate the molding system and melt flowing behaviors in an easy-to-understand way. The practical examples show how to use CAE to achieve design verification and process innovation in conventional injection molding, G/WAIM, co-/bi-injection, foam injection molding, PIM, RTM, and IC packaging. With this book, readers can effectively learn molding simulation applications and its importance in molding industries.

The CAE case study exercises found in the book for execution in the Moldex3D software can be downloaded from the Website: <https://moldex3d.box.com/s/zr6fvc1vlhbi4ocx111jwd3wmxt4ooif>, for which the QR code is as follows:



*Maw-Ling Wang*

*Rong-Yeu Chang*

*Chia-Hsiang (David) Hsu*

March 2022

# Contents

<b>Acknowledgments</b> .....	<b>V</b>
<b>Preface</b> .....	<b>VII</b>
<b>1 Overview of Plastics Molding</b> .....	<b>1</b>
<i>Che-Ping (Barton) Lin</i>	
1.1 Introduction to Injection Molding .....	1
1.1.1 The Systems of Injection Molding .....	3
1.1.1.1 The Cycle of Injection Molding .....	3
1.1.1.2 Injection Machine .....	4
1.1.2 Defects in Injection Molded Products .....	10
1.1.2.1 Short Shot .....	10
1.1.2.2 Warp .....	11
1.1.2.3 Flash .....	11
1.1.2.4 Sink Mark and Void .....	12
1.1.2.5 Air Trap .....	13
1.1.2.6 Burn Mark .....	13
1.1.2.7 Delamination .....	14
1.1.2.8 Fish Eye .....	14
1.1.2.9 Flow Mark .....	14
1.1.2.10 Stress Mark .....	15
1.1.2.11 Hesitation .....	15
1.1.2.12 Jetting .....	16
1.1.2.13 Splay .....	16
1.1.2.14 Weld Line .....	17

1.2	Core Values of Molding Simulation .....	18
1.2.1	Application of CAE Technology in Injection Molding .....	19
<b>2</b>	<b>Material Properties of Plastics .....</b>	<b>23</b>
	<i>Chen-Chieh (Jye) Wang</i>	
2.1	Overview .....	23
2.2	Rheological Properties .....	25
2.2.1	Viscosity .....	26
2.2.1.1	Effects of Non-Newtonian and Molecular Conformation .....	27
2.2.1.2	Effects of Shear Rate .....	28
2.2.1.3	Effects of Temperature .....	30
2.2.1.4	Effects of Pressure .....	31
2.2.1.5	Theoretical Models .....	31
2.2.1.6	Viscosity Properties of Plastics .....	33
2.2.2	Viscoelastic Fluids .....	35
2.2.2.1	Viscoelastic Behavior .....	35
2.2.2.2	Theoretical Models .....	37
2.2.2.3	Measurement of Viscoelasticity .....	41
2.3	Thermodynamic and Thermal Properties .....	46
2.3.1	Specific Heat Capacity .....	46
2.3.2	Melting Point and Glass Transition Temperatures .....	48
2.3.3	PVT Equation of State .....	49
2.3.3.1	Definition .....	49
2.3.3.2	Data Interpretation .....	50
2.3.3.3	Theoretical Models .....	51
2.3.3.4	Effects of Non-Equilibrium State on PVT .....	54
2.3.4	Thermal Conductivity and Heat Transfer Coefficient .....	56
2.3.4.1	Definition .....	56
2.3.4.2	Theoretical Models .....	57
2.3.4.3	Data Interpretation .....	57
2.3.4.4	Mold-Melt Contact and Heat Transfer Coefficient (HTC) .....	58

2.4	Mechanical Properties .....	59
2.4.1	Stress and Strain of Plastics .....	59
2.4.2	Solid-Like Viscoelasticity .....	60
2.4.3	Theoretical Model .....	61
2.4.4	Data Interpretation .....	62
2.5	Kinetic Properties .....	64
2.5.1	Crystalline .....	64
2.5.2	Theoretical Models .....	64
2.5.3	Effects of Cooling Rate on Crystallization .....	65
2.6	Curing Kinetics .....	66
2.6.1	Curing Phenomenon .....	66
2.6.2	Theoretical Models .....	67
2.6.3	Curing Effect on Viscosity .....	68
2.6.4	Data Interpretation .....	70
<b>3</b>	<b>Part and Mold Design .....</b>	<b>73</b>
	<i>Tsai-Hsin (Sam) Hsieh, Yao-Chen (Cloud) Tsai, Yao-Wei (Willie) Chuang</i>	
3.1	Part Design .....	73
3.1.1	Golden Rule: Uniform Wall Thickness .....	73
3.1.2	Wall Thickness versus Flow Length .....	76
3.1.3	Radius/Fillets and Chamfer Angle .....	78
3.1.4	Rib and Boss .....	79
3.1.5	Draft Angle .....	84
3.1.6	Design for Manufacturing (DFM) .....	85
3.1.7	Summary .....	86
3.2	Mold Design .....	87
3.2.1	Basics .....	88
3.2.2	Gate Design .....	91
3.2.2.1	Gate Number .....	91
3.2.2.2	Gate Location .....	92
3.2.2.3	Gate Types .....	95
3.2.3	Runner Design .....	97
3.2.3.1	Runner Shape and Dimension .....	98
3.2.3.2	Multi-Cavity Runner Design .....	99

3.2.4	Cooling Design .....	100
3.2.5	Others .....	102
3.2.5.1	Ejector System .....	102
3.2.5.2	Venting Design .....	102
<b>4</b>	<b>Process Conditions .....</b>	<b>105</b>
	<i>Chuan-Wei (Arvid) Chang</i>	
4.1	Introduction to the Injection Molding Cycle .....	105
4.1.1	Brief Introduction to Injection Molding Machine Units .....	105
4.1.2	Injection Molding Cycle .....	107
4.1.3	Molding Window .....	110
4.1.4	PVT Variations during Injection Stages .....	111
4.2	Plasticizing Conditions .....	122
4.2.1	Nozzle Temperature and Cylinder Temperatures .....	122
4.2.2	Back Pressure, Screw rpm, Suck Back, and Metering Stroke ..	123
4.3	Filling Conditions .....	129
4.3.1	Filling Time versus Injection Velocity .....	129
4.3.2	Injection Pressure .....	133
4.3.3	VP Switch .....	136
4.4	Packing Conditions .....	138
4.5	Cooling Conditions .....	140
4.5.1	Cooling Time .....	140
4.5.2	Coolant Flow Rate .....	141
4.5.3	Mold Temperature .....	141
4.6	Connecting Smart Design to Smart Manufacturing .....	142
4.6.1	Machine Characterization .....	143
4.6.2	The CAE Setting Mode in Combination with Injection Machine on Site .....	148
4.6.3	Case Study .....	150
<b>5</b>	<b>Molding Simulation Methodology .....</b>	<b>157</b>
	<i>Hsien-Sen (Ethan) Chiu</i>	
5.1	The Goal of Molding Simulation .....	157
5.1.1	Design Verification and Optimization .....	158

5.1.1.1	Overview of Design for Manufacture (DFM) . . . . .	158
5.1.1.2	CAE and DFM: A Practical Case Study . . . . .	160
5.1.2	Process Conditions Optimization . . . . .	167
5.1.2.1	Molding Stability . . . . .	167
5.1.2.2	Real Case . . . . .	169
5.2	Basics of Simulation Equations . . . . .	173
5.2.1	Governing Equations . . . . .	174
5.2.2	Numerical Approximation . . . . .	175
5.2.2.1	Finite Difference Method (FDM) . . . . .	175
5.2.2.2	Finite Volume Method (FVM) . . . . .	178
5.2.2.3	Finite Element Method (FEM) . . . . .	180
5.3	What Is Molding Simulation? . . . . .	182
5.3.1	Brief History of Molding Simulation . . . . .	182
5.3.2	Simulation Workflow . . . . .	189
<b>6</b>	<b>Flow Consideration versus Part Features . . . . .</b>	<b>193</b>
	<i>Wen-Hsin (Debbie) Weng</i>	
6.1	Basics . . . . .	193
6.1.1	Flow Behavior of Plastic Melt in the Cavity . . . . .	193
6.1.2	Effects of Filling Time . . . . .	198
6.1.3	Flow Rate versus Injection Pressure . . . . .	199
6.1.3.1	Flow Rate Curve Setting . . . . .	199
6.1.3.2	Relationship of Injection Rate and Injection Pressure . . . . .	203
6.1.4	VP Switch and Cavity Pressure . . . . .	209
6.1.5	Effects of Part Thickness . . . . .	218
6.1.6	Material Viscosity an Flow Behaviour . . . . .	223
6.1.7	Summary . . . . .	227
6.2	Practical Applications . . . . .	228
6.2.1	CAE Solution to Stress Mark in a Phone Shell . . . . .	228
6.2.2	Flow Rate Effect on Injection Pressure of Laptop Product . . . . .	232
6.3	CAE Case Study . . . . .	234

<b>7</b>	<b>Runner and Gate Design</b> .....	<b>239</b>
	<i>Yao-Chen (Cloud) Tsai, Yao-Wei (Willie) Chuang</i>	
7.1	Basics .....	239
7.1.1	General Design Guide of Runners .....	239
7.1.2	General Design Guide of Gates .....	244
7.1.3	Gate Sealing .....	256
7.1.4	Flow Balance .....	258
7.2	Practical Applications .....	265
7.2.1	CAE Verification on MeltFlipper® Design .....	265
7.2.2	CAE Verification of Multi-Cavity Systems .....	271
7.3	CAE Case Study .....	275
<b>8</b>	<b>Cooling Optimization</b> .....	<b>279</b>
	<i>Hung-Chou (Kent) Wang</i>	
8.1	Basics .....	279
8.1.1	Heat Transfer Mechanism .....	280
8.1.2	Design Golden Rule: Uniform Mold Temperature .....	283
8.1.3	General Design Guide of Cooling Channel .....	287
8.1.4	Cooling Efficiency: Coolant Flow Consideration .....	291
8.1.5	Cooling Time Estimate .....	294
8.1.6	Use CAE Cooling Analysis .....	296
8.1.7	Conformal Cooling Application .....	299
8.2	Practical Applications .....	303
8.2.1	Digital Camera Cover .....	303
8.2.2	Cartridge .....	308
8.3	CAE Case Study .....	312
<b>9</b>	<b>Warpage Control</b> .....	<b>315</b>
	<i>Shih-Po (Tober) Sun, Wen-Hsin (Debbie) Weng</i>	
9.1	Basics .....	315
9.1.1	The Causes of Warpage .....	318
9.1.2	Material Effects .....	321
9.1.3	Geometrical Effects .....	324
9.1.4	Process Condition Effects .....	326



9.1.5	Criteria of CAE Warp Analysis .....	328
9.1.6	Methods to Minimize Warpage .....	332
9.2	Practical Applications .....	338
9.3	CAE Case Study .....	343
<b>10</b>	<b>Fiber Orientation Control .....</b>	<b>347</b>
	<i>Huan-Chang (Ivor) Tseng</i>	
10.1	Basics .....	348
10.1.1	Process Principle .....	350
10.1.2	Theory Models .....	351
10.1.3	Advantages and Challenges .....	361
10.2	Practical Applications .....	362
10.2.1	Using the iARD-RPR Model for an Injection Molded Center-Gated Disk with Fiber-Reinforced Thermoplastics .....	362
10.2.2	Comparison of iARD-RPR Models under GNF Decoupling and IISO Coupling .....	366
10.2.3	The Influences of Material Flow and Fiber Interaction on Fiber Orientation and Product Quality during Injection Molding .....	369
10.3	CAE Case Study .....	374
<b>11</b>	<b>Hot Runner Optimization .....</b>	<b>379</b>
	<i>Tsai-Hsin (Sam) Hsieh</i>	
11.1	Basics .....	379
11.1.1	Process Principle .....	380
11.1.2	Temperature Control in a Hot Runner System .....	384
11.1.3	Advantages and Challenges .....	386
11.2	Practical Applications .....	395
11.2.1	CAE Verification on a Single-Gate Hot Runner System .....	395
11.2.2	CAE Pin Movement Control of Valve Gate .....	404
11.3	CAE Case Study .....	408

<b>12</b>	<b>Co-/Bi-Injection Molding</b> .....	<b>411</b>
	<i>Chih-Chung (Jim) Hsu, Yu-Sheng (Tim) Chou</i>	
12.1	Basics .....	412
12.1.1	Process Principle .....	412
12.1.2	Advantages and Challenges .....	415
12.1.3	Theory Models .....	417
12.2	Practical Applications .....	418
12.2.1	Co-Injection Molding of Fork Model .....	418
12.2.2	Co-Injection Molding: Core Breakthrough and Flow Imbalance .....	420
12.2.3	Co-Injection Molding: Fiber Orientation Predictions .....	424
12.2.4	CAE Case of Bi-Injection Molding .....	426
12.3	CAE Case Study .....	430
<b>13</b>	<b>Gas-/Water-Assisted Injection Molding</b> .....	<b>433</b>
	<i>Chih-Chung (Jim) Hsu, Yu-Sheng (Tim) Chou</i>	
13.1	Basics .....	433
13.1.1	Process Principle .....	434
13.1.1.1	Short-Shot Process .....	434
13.1.1.2	Full-Shot Process .....	436
13.1.2	Advantages and Challenges .....	438
13.2	Practical Applications .....	446
13.2.1	CAE Verification on GAIM .....	446
13.2.2	CAE Verification on WAIM .....	449
13.2.3	CAE Verification on GAIM: Fingering Effect .....	452
13.3	CAE Case Study .....	454
<b>14</b>	<b>Foam Injection Molding</b> .....	<b>457</b>
	<i>Yuan-Jung (Dan) Chang, Li-Yang (Robert) Chang, Chih-Wei (Joe) Wang</i>	
14.1	Basics .....	457
14.1.1	Microcellular Process Principle .....	458
14.1.2	Advantages and Challenges .....	462
14.1.3	Theory Models .....	464

14.2	Practical Applications .....	466
14.2.1	CAE Verification on Microcellular Injection Molding: Case 1 ..	466
14.2.2	CAE Verification of Microcellular Injection Molding: Case 2 ..	473
14.2.3	CAE Verification on Chemical Foaming Injection Molding ....	480
14.2.4	CAE Verification of Polyurethane Reactive Foaming Molding ..	483
14.2.5	Summary .....	491
14.3	CAE Case Study .....	492
<b>15</b>	<b>Powder Injection Molding .....</b>	<b>495</b>
	<i>Huan-Chang (Ivor) Tseng</i>	
15.1	Basics .....	495
15.1.1	Process Principle .....	496
15.1.2	Advantages and Challenges .....	497
15.1.3	Theory Models .....	500
15.2	Practical Applications .....	505
15.3	CAE Case Study .....	508
<b>16</b>	<b>Resin Transfer Molding .....</b>	<b>511</b>
	<i>Hsun (Fred) Yang, Yu-He (Zoe) Chen</i>	
16.1	Basics .....	512
16.1.1	Process Principle .....	516
16.1.2	Advantages and Challenges .....	520
16.2	Theory Models .....	521
16.2.1	2.5D Analysis .....	521
16.2.2	3D Analysis .....	523
16.2.3	Measurement of Permeability .....	525
16.2.4	Porosity .....	528
16.2.5	Measurement of Chemorheological Properties .....	529
16.2.6	Simulation Parameters .....	530
16.3	Practical Applications .....	531
16.3.1	CAE Verification on Edge Effects .....	531
16.3.2	CAE Verification on Thickness-Direction Flow .....	533
16.3.3	CAE Verification on a Wind Turbine Blade .....	538
16.3.4	CAE Verification on Mat Effects .....	540

16.3.5 CAE Verification on Flybridge ..... 543

16.4 CAE Case Study ..... 547

**17 Integrated Circuit Packaging ..... 549**

*Chih-Chung (Jim) Hsu, Chia-Peng (Victor) Sun, Chen-An (Jennan) Wang, Yu-En (Joseph) Liang*

17.1 Basics ..... 549

17.1.1 Process Principle ..... 554

17.1.2 Advantages and Challenges ..... 557

17.1.3 Theoretical Models ..... 559

17.2 Practical Applications ..... 563

17.2.1 CAE Verification on Void Prediction ..... 563

17.2.2 Fluid-Structure Interactions: Wire Sweep Analysis ..... 567

17.2.3 Fluid-Structure Interactions: Paddle Shift and Chip Deformation Analysis ..... 569

17.2.4 Warpage Prediction for a Bilaminate ..... 577

17.2.5 Warpage Prediction for a Bi-Material Component Model ..... 580

17.2.6 Warpage of Bi-Material Strip ..... 583

17.2.7 The Effect of Dispensing Control and Creeping Behavior on the Underfill Process ..... 586

17.3 CAE Case Study ..... 591

**Index ..... 595**

# Overview of Plastics Molding

Che-Ping (Barton) Lin

The context of plastics molding will be briefly introduced in this chapter using the most popular method of injection molding. Two major topics are included in this chapter:

1. Introduction to Injection Molding: The systems of injection molding and the defects of injection molded products are described.
2. Core Values of Molding Simulation: The core values of simulation in injection molding will be introduced at the end of this chapter.

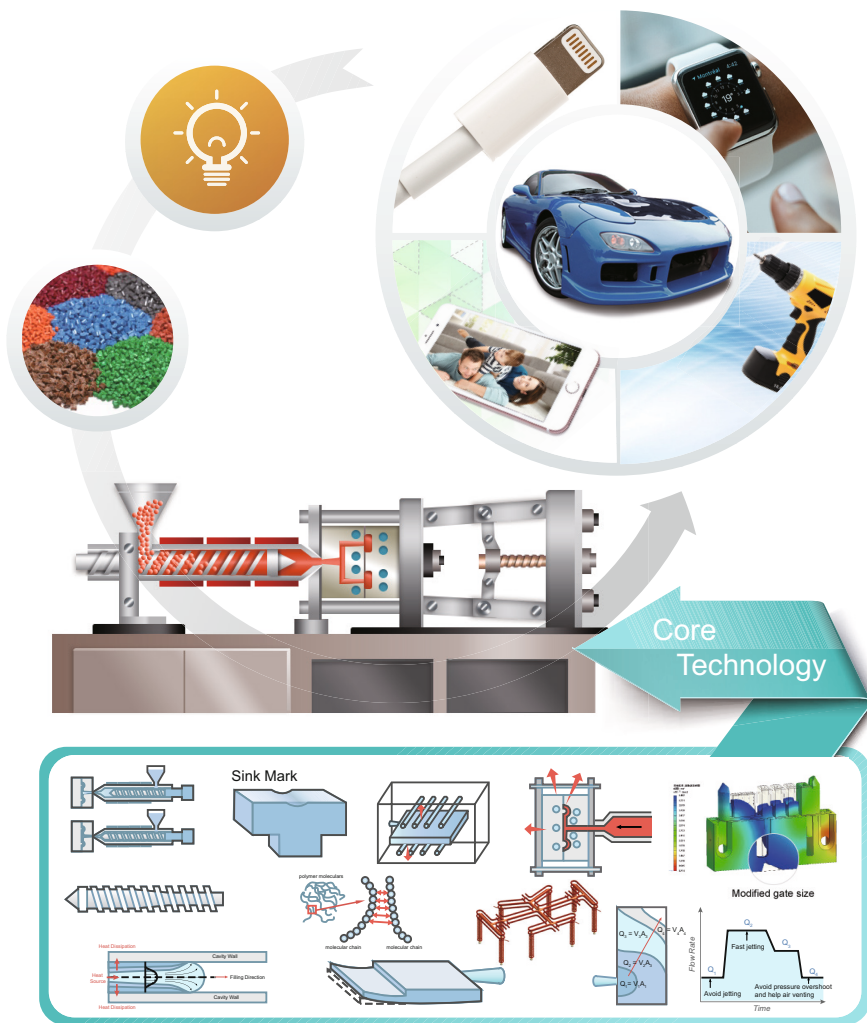
## ■ 1.1 Introduction to Injection Molding

Plastics can be shaped because of their ductility and plasticity. Therefore, plastics have been widely used in daily life and become a necessary part of the current world. The source of plastic products comes from customers' "needs", which are then developed to "design concepts". Such design concepts will be delivered to product designers for product design before being handed over to mold designers for mold design and development, as shown in Figure 1.1.

There are four stages from product development to mass production:

1. Design product drawings according to its functions, appearance, material, and processes, and hand over to mold factories for the design and manufacturing of molds.
2. Mold designers undertake discussion, drawing design, machining, mold-closing, and other procedures upon receiving product drawings, samples, or relevant specifications regarding material, weight, color, etc., which are used to manufacture the molds based on the conclusions made in the mold manufacturability meeting. The manufactured molds will be delivered to molding factories for mold test, modification, and detection.

3. Molding engineers execute tests to obtain better molding conditions for smooth production during the mold test stage, and provide feedback comments for mold modification regarding the difficult points for molding. The mold test will be executed repeatedly after the mold modification until the product quality achieves the specification of the mold test.
4. The production yield is improved via small-scale production and quality certification before the mass production stage begins. To obtain high-quality plastic products, one must first understand the relevant principles and mechanisms of the molding process. This section will briefly introduce the most common components of injection molding systems.

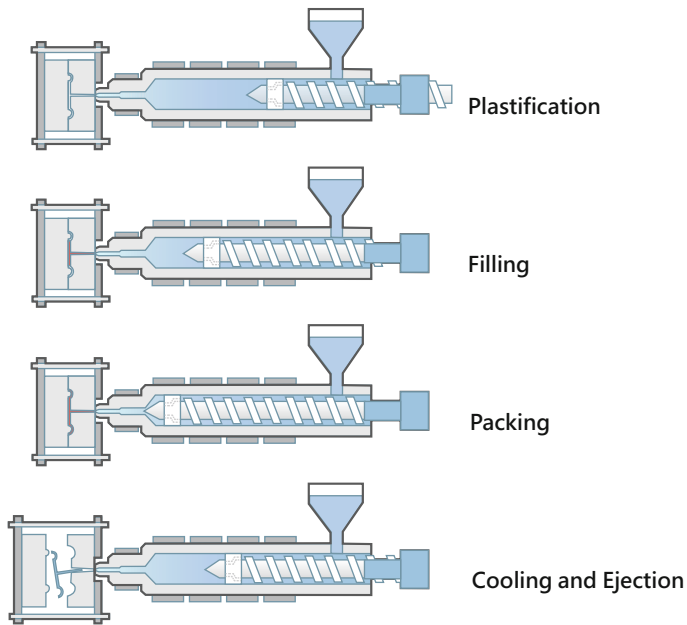


**Figure 1.1** Development of workflow of mold products

## 1.1.1 The Systems of Injection Molding

### 1.1.1.1 The Cycle of Injection Molding

First, what is injection molding? Simply speaking, it is a process of making a product by injecting plastic material of liquid state into a mold cavity via the help of injection molding machines. When the plastic material enters the injection molding machine through a hopper, it is turned into a melted state after being squeezed by the screw from which a large amount of heat is generated through friction. The melted plastic accumulates in the front of the cylinder and is constantly heated in order to maintain the temperature for injection. The process mentioned above is called plastification, as shown in Figure 1.2.



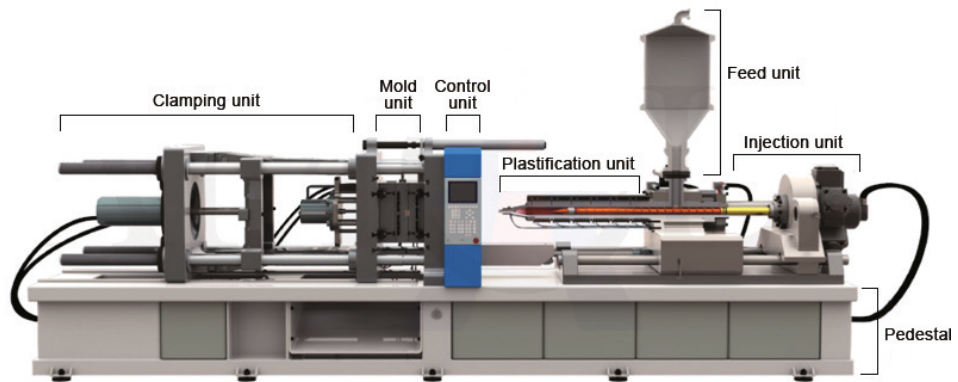
**Figure 1.2** Cycle of injection molding

Then, the melted plastic will be pushed forward into the closed mold cavity by the screw, a process that is called injection. After the initial injection is completed, when the high molecular weight melted plastic has fully filled the mold cavity, more melted plastic is injected under high pressure in order to compensate for the decrease in the volume of the plastic due to cooling as well as to make sure the mold cavity is perfectly filled until the sprue is solidified, a process that is called packing. Finally, the movable side moves back until the ejection pin reaches the rear platen to eject the molded product, runner system, and waste. This cycle is known as the molding cycle of injection molding.

### 1.1.1.2 Injection Machine

Figure 1.3 shows a basic injection molding machine (injection machine), which is suitable for manufacturing products of different shapes from thermoplastic or thermosetting plastics. There are two basic functions: 1) heating of the plastics to a melted state, and 2) application of high pressure to inject the melted plastic to fill the mold cavity completely.

Injection machine systems often have different components due to different types and uses, but generally comprise injection unit, clamping unit, mold unit, plastification unit, feed unit, and control unit.



**Figure 1.3** Injection machine

In industrial plastics processing methods, whether extrusion, injection, calendering, blow molding, film blowing, or spinning, a huge quantity of additional auxiliary equipment is always required to complete each processing step. The optimization, automation, and rationalization of auxiliary equipment for plastics processing play a role in determining product quality and the economic viability of the process.

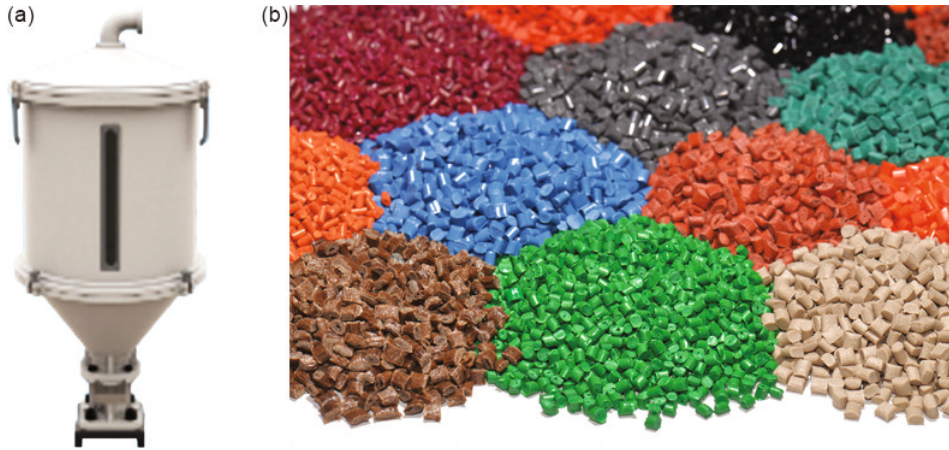
Next, we will introduce the equipment required for injection molding in detail. This includes the feed, control, plastification, injection, and mold systems.

#### 1.1.1.2.1 Feed System

Generally, there are two kinds of feed systems, namely independent and central. Independent feed equipment is usually set above the feeding port of the injection machine, i.e. the hopper with inverted cone structure, as shown in Figure 1.4(a). Some are supplemented by a heating or drying device, and also with a metering device to quantify the plastics, as shown in Figure 1.4(b).



The other kind of central feed system (also called automatic feed system or centralized feed system), including suction machine, central material loader, and conveying control system, has the advantages of continuous feeding, centralized automatic control, uniform mixing, and flexibility to change colors.



**Figure 1.4** (a) Hopper and (b) plastic pellets

#### 1.1.1.2.2 Control System

The control system (Figure 1.5) can be said to be the brain and nerve center of the entire injection machine. The pressure, temperature, speed and time of the machine are controlled via the set values input by the operator that will directly affect the molding cycle and product quality.

The key physical parameters of injection molding processing are temperature, pressure, speed, time, and position, each of which includes the following:

1. Temperature includes resin drying temperature, barrel temperature, melt temperature, mold temperature, machine oil temperature, and working environment temperature.
2. Pressure includes filling pressure, holding pressure, back pressure, ejection pressure, mold opening pressure, and mold clamping pressure.
3. Speed includes injection speed, screw rotation speed, mold opening and closing speeds, and ejection speed.  
Time includes filling time, pressure holding time, cooling time, and resin drying time.
4. Position covers measuring position, VP switch position, eject position, and switch mode position.



Figure 1.5 Control panels from Nissei and Arburg

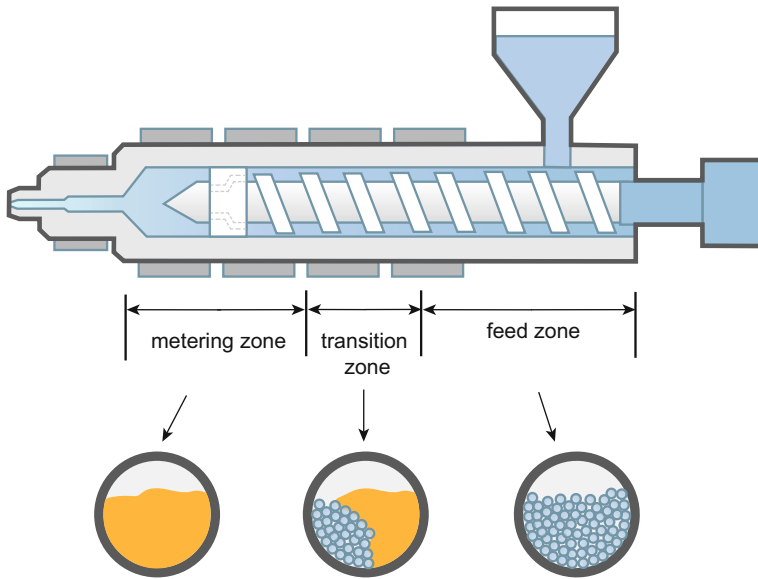
One of the biggest problems encountered in common development and quality control of molded products during the production process is ineffective quality control due to using a one-way, indirect method for operating injection machines and system control devices. Therefore, it is important to analyze the characteristics of the machines so as to understand the different ways in which they can be used to exert good control over the process conditions.

#### 1.1.1.2.3 Plastification System

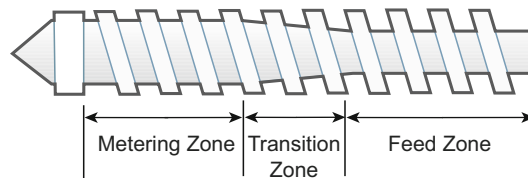
Plastification is a process that uses the mechanical energy of the screw and the thermal energy of the heater to melt the incoming solid plastic, which is then applied with high pressure to be ready for injection. The plastic is turned into a melted state after being squeezed by the screw from which a large amount of heat is generated through friction. The melted plastic accumulates in the front of the cylinder and is constantly heated in order to maintain the temperature.

As shown in Figure 1.6 and Figure 1.7, the solid plastic enters the screw channel via the inlet hopper. With the high rotation speed of the screw that generates a shear stress effect with the barrel, the plastic is mixed and transferred along the screw channel. As the solid plastic is heated by the electric heaters outside the

barrel and due to the shear stress effect, it turns into a melted state as the temperature rises inside the barrel.



**Figure 1.6** Barrel and plastification



**Figure 1.7** Screw

The screw is divided into three zones (Figure 1.7):

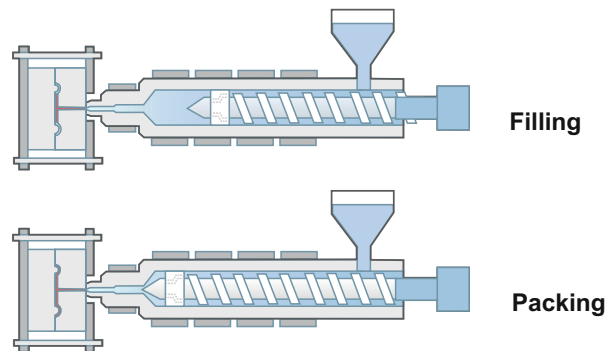
1. **Feed zone:** The fixed feed depth of the screw channel is for pre-heating, transferring, and pushing the plastic granules, which start to melt at the end of the feed zone.
2. **Transition zone:** The thread depth is gradually decreased in the transition zone, the purpose of which is melting, mixing, shearing, and compressing of the plastic, and pressurized venting. The plastic must be completely melted in this zone. The volume of the melted plastic will be reduced and should be compressed accordingly to avoid incomplete compression and poor venting.
3. **Metering zone:** The fixed metering depth of the screw channel is for transfer and metering of the melted plastic, as well as providing sufficient pressure to

maintain a uniform temperature and stabilize the flow of the melted plastic. The length of this zone greatly affects the quality of the melt injected into the mold cavity. The longer the metering zone, the better is the chain mixing result. But a zone that is too long will cause a long dwell time of the melt in the barrel and will induce thermal decomposition. In contrast, a zone that is too short will lead to an uneven melt temperature.

The length and geometry of the zones in the screw directly affect the extent of plastification and the transport efficiency of the plastic. Judicious screw selection is very important for injection molding.

#### 1.1.1.2.4 Injection System

The injection system is mainly responsible for filling and packing (Figure 1.8). For the filling stage, the screw moves forward to inject the melted plastics into the closed mold cavity through the nozzle to finish the filling process. When the melted plastic enters the cavity, the air is expelled from the ejection pin, parting line, and vent holes. Under-injection would occur if the liquidity is poor or the injection pressure is insufficient; in contrast, if the liquidity is too high, flash (see Section 1.1.2.3) would occur on the parting facet of the plastic part.



**Figure 1.8** Injection system

After the mold cavity has been almost filled by the melt in the filling stage, the machine continues to apply high pressure to inject more melt into the mold cavity, to pre-compensate for the plastic volume shrinkage caused by cooling and to ensure that the melt completely fills the mold in the packing stage. Packing continues until the gate is sealed or the packing time ends.

#### 1.1.1.2.5 Mold System

The mold system generally includes a fixed side and a movable side platen. The space inside the platens is the mold cavity, and is where the plastic is molded into shape. The mold also consists of ejection mechanisms such as ejector pins or ejector platens for ejecting the solidified product from the cavity. A typical structure is shown in Figure 1.9.



**Figure 1.9** Open mold

Molds are important in injection molding. The basic structure of a mold is generally divided into three types: two-platen mold, three-platen mold, and hot runner. The decision for a particular mold structure is generally made by customers or according to products. A plastic mold consists of seven major systems: guiding, support, molding component, pouring, cooling, ejection, and venting systems. Using a sliding block is a way to handle undercuts, but normally the mechanism of mold opening and closing is sufficient for lateral parting, core extracting, and position reset.

A complete cycle time of plastics injection molding consists of filling, packing, cooling, and mold opening times, among which the cooling time has the highest proportion at about 70–80%. Therefore, the design of cooling system is a critical step which directly affects the length of cycle time, production efficiency, and cost. The following chapters will introduce the characteristics of plastic processing and the key points of mold design in detail.

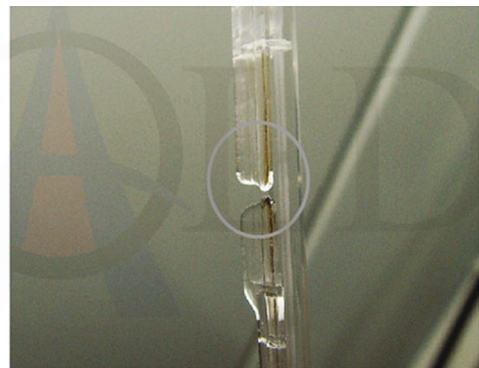
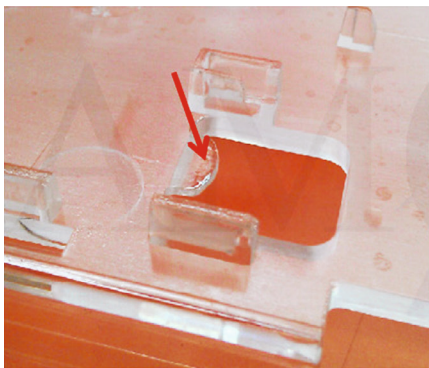
### 1.1.2 Defects in Injection Molded Products

Product defects present another concern when plastic is turned into the final product through the foregoing processes. The plastic takes its shape gradually through the cooling during the process of injection molding, and usually it has the form of a near-finished product when it leaves the mold. If there are defects in the plastic product, it is necessary to analyze and understand the factors that are the cause.

The common injection molding defects are briefly described as follows:

#### 1.1.2.1 Short Shot

The phenomenon called the “short shot”, shown in Figure 1.10, gives a defective appearance to the final plastic product, and is caused by under-filling of the mold cavity. It is most apparent at in thinner zones or at the end of runners, and is mainly caused by insufficient plastic supply or poor liquidity of the plastic itself, so that the liquid state halts prematurely during the filling process. Therefore, any factor that affects the smooth flowing of the melted plastic is likely to cause short shot defects, such as insufficient amount of plastic injected, too high flow resistance, or insufficient liquidity.



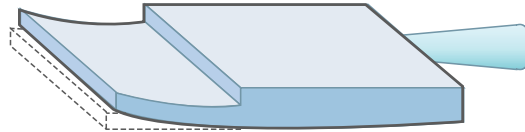
**Figure 1.10** Short shot

In addition to a low temperature of melted plastic and mold wall, a thin part geometry or improper sprue location or length can also generate short shot defects as the mold cavity cannot be filled up. Improper configuration of the vent hole is also likely to cause a short shot.

It should be confirmed that the hopper has enough plastic if a short shot is observed. Then, the cylinder should be checked for blockage and the back-pressure valve checked for failure, which can result in a low injection pressure or material leakage. However, a long injection time can also cause a short shot.

### 1.1.2.2 Warp

Warp denotes the distortion or deformation of a product after injection molding. It is the defect type most commonly seen in injection molded products. Figure 1.11 shows a warped finished product which has two parts that cannot be assembled together. However, even if the product is not a combinative part but a single product, warp can also give rise to customer complaints and product returns. Therefore, product warp should be strictly controlled to within the tolerance.



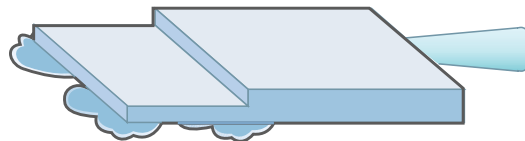
**Figure 1.11** Warp resulting in a molded product that cannot be fitted

Thermal expansion and contraction are also seen in plastics. The melted plastic starts to cool down and solidify as it enters the mold cavity, and it contracts during the process of cooling and solidification. If the contraction rate is evenly distributed across the product, warp would not be seen and only shrinkage would result. However, with the interaction between the external factors, e.g. molding conditions, mold cooling design, product appearance design, and the plastics characteristics, e.g. molecular chain and fiber orientation, it is very difficult for plastic finished products to contract evenly or with low contraction rate.

It can be seen from the above that the causes of warp are various, complicated, and interdependent. Ways of reducing warp are a very important concern for producers.

### 1.1.2.3 Flash

Flash is generated as there is a gap existing at the split plane via which the melted plastics spills outside the mold cavity, as shown in Figure 1.12.



**Figure 1.12** Flash

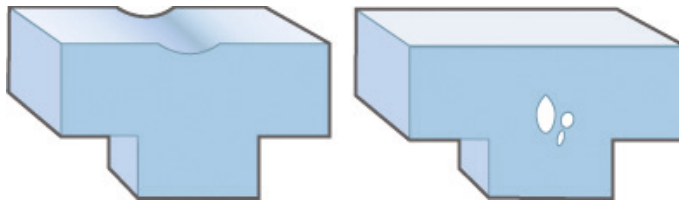


The main causes of such formation are as follows:

1. Mold clamping force is too small: A pushing force is applied to the mold by the melted plastics during the injection molding process, especially if the central area of the mold cavity is subjected to excessive high pressure the mold will separate from the parting plane.
2. Mold gap: The causes that the moving and stationary side of the mold cannot contact completely consist of a) a parting plane that is defective and not parallel between each side, and b) impurities on the parting plane that create gaps on the parting plane.
3. Improper molding conditions: Wrong choice of molding machine, over-temperature of melted plastics, and excessive injection pressure are all causes of flash generation.
4. Improper venting system: Flash will be generated if the venting is insufficient or the venting groove is too deep.

#### 1.1.2.4 Sink Mark and Void

The formation of sink marks and voids is a phenomenon observed in thick areas where there is not enough plastic supplied during the cooling process, as shown in Figure 1.13.



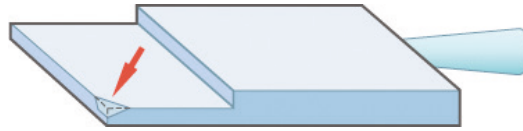
**Figure 1.13** Sink mark/void

Sink marks are generated as the plastic contacting the mold walls cools and hardens before the inner plastic starts to cool down, and hence the surface is pulled inward by contraction. If the surface strength is sufficient, voids are generated instead of sink marks. Therefore, sink marks and voids are often seen at the rib parts or the backside of a convex surface. In conclusion, sink marks and voids are generated easily if the contraction is uneven between the inner and outer part in some areas.



### 1.1.2.5 Air Trap

Air trap denotes a condition in which the melt front of the melted plastic traps the air inside the mold cavity, so that the air cannot escape from the venting holes or the gaps in the mounting parts. A possible consequence is shown in Figure 1.14.

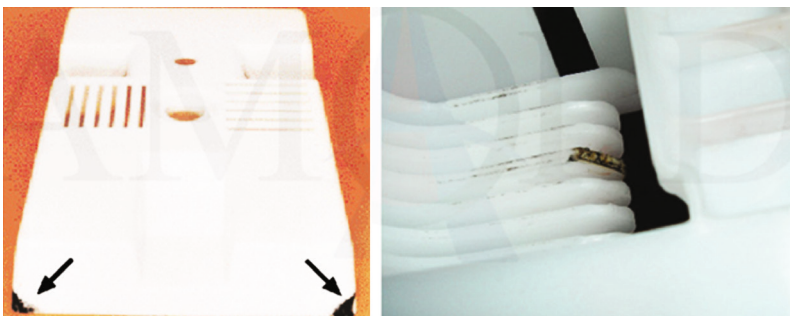


**Figure 1.14** Air trap

Generally speaking, air trap mostly occurs in the area filled last, where there is no venting hole or the venting holes are too small, with the result that bubbles, short shot, or surface defects are generated inside the plastic part. In addition, any large difference in the thickness of the parts will lead the melt flows toward the thicker area instead of the thinner area, giving rise to the race-tracking effect, which is also one of the reasons for air trap.

### 1.1.2.6 Burn Mark

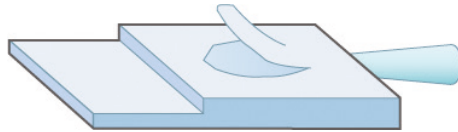
The causes of burn marks are very similar to those of air traps. The major cause is that the air trapped inside the mold cavity is overheated by compression and creates dark marks on the plastic surface as shown in Figure 1.15. When the air inside the mold cavity is compressed, the pressure and temperature rise so rapidly that the surface of the plastic part at the end of the flowing path is decomposed and thereby burn marks are generated. Generally, burn marks usually occur in tandem with air traps.



**Figure 1.15** Burn mark

### 1.1.2.7 Delamination

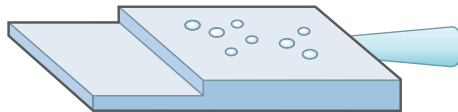
The main cause for delamination (layer separation) is due to the mixing of two incompatible materials or material types used in the molding process that are too dissimilar, as shown in Figure 1.16. In addition, delamination is also possible to occur if the temperature of the melted plastic is too low, the humidity of the material is too high, or the runner and sprue are not smooth.



**Figure 1.16** Delamination

### 1.1.2.8 Fish Eye

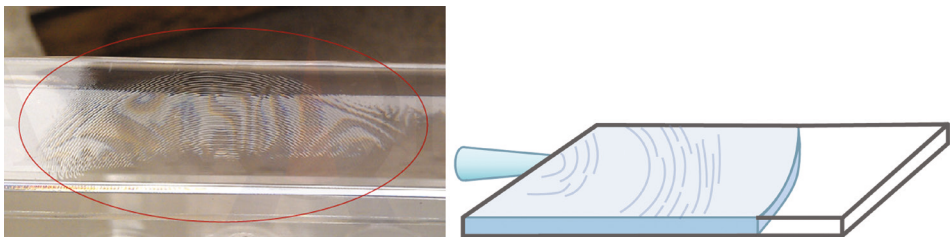
Fish eyes, as shown in Figure 1.17, are usually caused by unmelted plastic because of insufficient cylinder temperature and screw rotating speed, and low backside pressure. The phenomenon can also result from using too much recycled material or contaminated plastic. Therefore, if the above-mentioned situation can be avoided, the probability of fish-eye occurrence can be effectively reduced.



**Figure 1.17** Fish eye

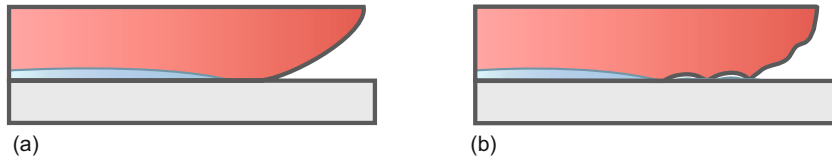
### 1.1.2.9 Flow Mark

Flow marks, as shown in Figure 1.18, are generated mainly if the temperature of the melted plastic is not evenly distributed or the viscosity of the melted plastic is excessively high.



**Figure 1.18** Flow mark

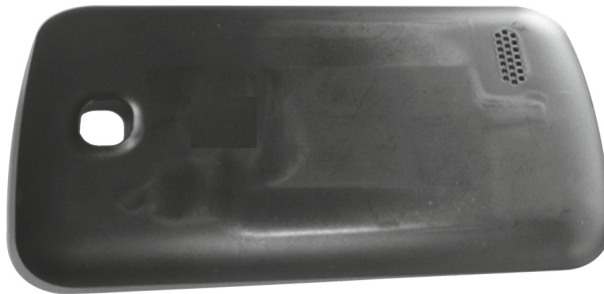
An excessively low temperature causes friction and pushing between the plastic and the mold cavity, and results in the plastic's hardening too quickly and leaving a flow mark, as shown in Figure 1.19. In addition, flow marks may occur if the melt near the gate solidifies due to unexpected cooling, or the melt is unable to provide compensation in the packing stage.



**Figure 1.19** (a) General fountain flow and (b) over-rapid cooling conditions that give rise to uneven local temperatures will readily cause flow marks

#### 1.1.2.10 Stress Mark

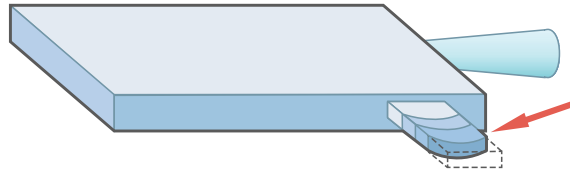
On the surface of the injection molded part, a shiny white mark occasionally appears and is called a stress mark. Generally speaking, a stress mark is induced by internal stress. If the thickness of a plastic part varies a lot, the cooling speed at a thinner area differs significantly from that of other areas. Then, the uncooled melted plastic will apply stress on the cooled plastics, which generates a stress mark due to inner stress, as shown in Figure 1.20.



**Figure 1.20** Stress mark

#### 1.1.2.11 Hesitation

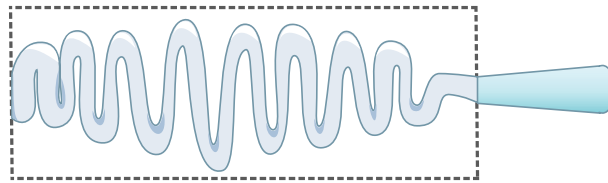
When the mold cavity is being filled, the melted plastic tends to move to a thicker and low-flow-resistance area, which it fills up first before filling the thinner area. Therefore, the melted plastic usually hardens at a stagnation point as the flow stops at the thinner area. It is highly possible for the solidified plastic to be pushed to the surface of the plastic part and create a hesitation mark when the following melted plastic starts to move to such a thinner area, as shown in Figure 1.21. In addition, hesitation often leads to short shots because the plastic usually completely solidifies at the stagnation point.



**Figure 1.21** Hesitation

### 1.1.2.12 Jetting

Jetting is usually generated when the melted plastic passes through a narrow sprue or runner into the mold cavity with a high speed, as shown in Figure 1.22. Jetting normally causes contact between cold materials as the temperature of the plastic strips injected into the mold cavity drops and the strips make contact with each other afterward. The strength of the plastic part will be reduced when jetting happens, which is more likely to cause surface and internal defects at the same time. Thus, jetting should be avoided as much as possible in order to assure production quality.



**Figure 1.22** Jetting

### 1.1.2.13 Splay

Splays, as shown in Figure 1.23, are caused by the incomplete release of humidity or other volatile gases mixed in the plastic melt during the plastification stage, or by gases generated from slight decomposition of the plastic due to an excessively high pre-heating temperature.

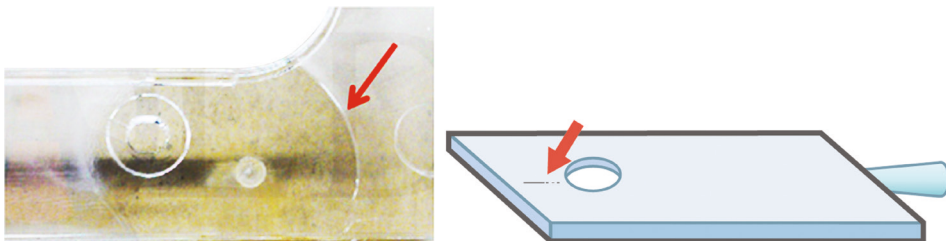
If the plastic is not properly dried before manufacturing, the moisture inside will evaporate into steam during injection filling, which causes bubbles to flow along with the melted plastics inside the mold cavity and thus silver stripes (splays) will occur along the flowing direction. If the bubbles cannot be expelled entirely upon completion of filling, splays will also occur on the surface of the plastic part.



**Figure 1.23** Splay

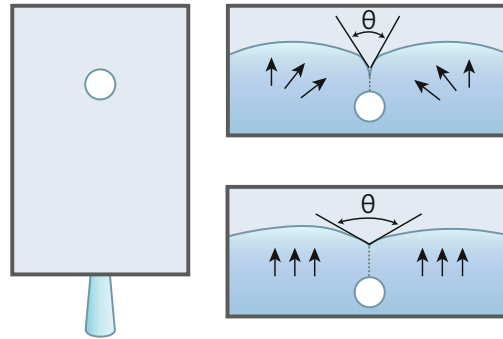
#### 1.1.2.14 Weld Line

When two or more plastic flow fronts merge together during the injection process, incomplete fusion can occur as the melt front is of lower temperature and hardens first. Hence, weld lines, as shown in Figure 1.24, are generated. Such defects are usually seen around the holes or the merging boundaries of the finished products. Therefore, when race-tracking effects take place, they are usually accompanied by weld lines. To avoid the generation of weld lines, extreme care should be taken regarding conditions such as significant thickness changes or multiple sprues in the mold.



**Figure 1.24** Weld line

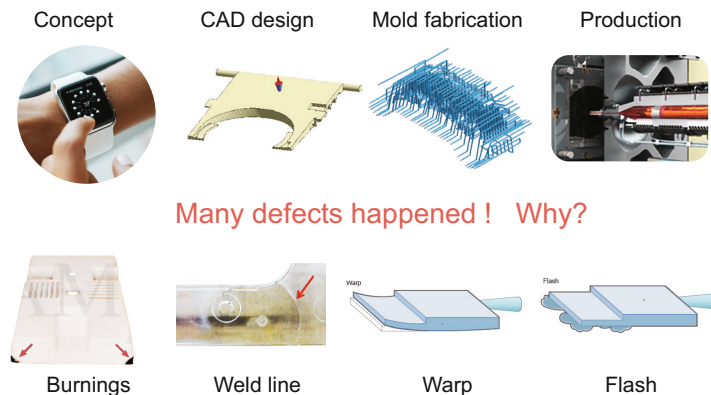
The plastic melts cannot be completely fused at the weld line, as a result of which the strength of the plastic part is lowered. Therefore, if weld lines cannot be avoided, the position and size of the gate should be adjusted to make the weld lines occur in as inconspicuous a low-stress area as possible. Generally, melt fronts converging from two directions at less than  $135^\circ$  will give rise to weld lines, as shown in Figure 1.25.



**Figure 1.25** The converging of melt fronts

## ■ 1.2 Core Values of Molding Simulation

From the foregoing introduction to plastics injection molding, it can be seen that the types of defects are of various kinds, which can be categorized as appearance or dimensional issues, as shown in Figure 1.26.



**Figure 1.26** Molding challenges: design quality

When facing these defect issues, the traditional solution is the trial-and-error method, i.e. to repeat mold test and mold modification until the product specifications are met, which usually takes gigantic amount of time, labor, and other costs. However, with the assistance of CAE (Computer Aided Engineering) tools, the production process becomes more efficient and the product quality gets better, while waste is further reduced, with environmental benefits. An introduction to CAE, including its application possibilities in injection molding, is given below.

### 1.2.1 Application of CAE Technology in Injection Molding

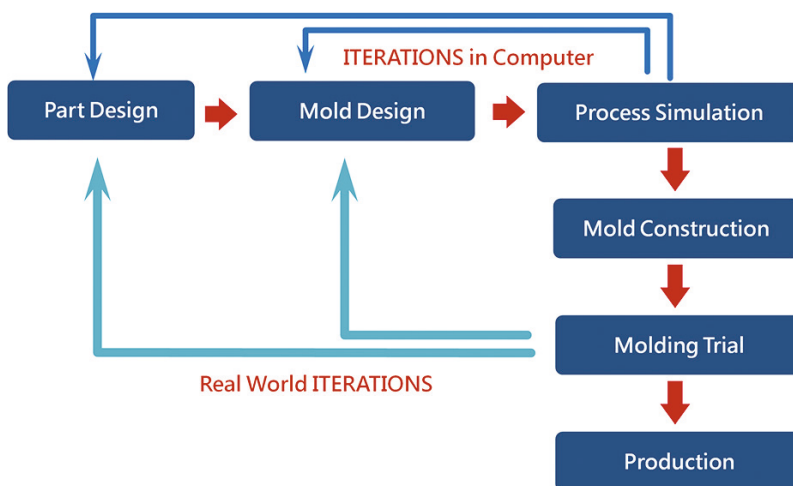
CAE is a kind of computer aided engineering software and technology that uses computer simulation and analysis to assist the diagnosis and development of complicated injection molding processes. CAE is able to integrate the complicated rheological, thermal, and mechanical properties of a material, and enables designers and developers to do qualitative and quantitative analysis and diagnosis for mold design as well as analysis and diagnosis for existing molds and operating conditions.

From the CAE analysis result, developers can explore the causes of problems that occur and test different design changes to find out the most appropriate solution, which is not achievable by the traditional trial-and-error method. Furthermore, if the design change involves modifications of products or molds, the cost of time, labor, machine, material, and energy by repeated mold tests and modifications is even beyond estimation. Hence, it is common to implement CAE for design verification during the development process.

We know that the injection process is a major factor that determines product quality. Going through solid, melted, and back to solid states in a short time involves rearrangement of plastic molecules. If we can effectively control the transition of plastic properties in the process, the structural strength of the product can be assured.

Where is CAE used?

CAE is not always suitable to provide assistance for injection molding, as shown in Figure 1.27.



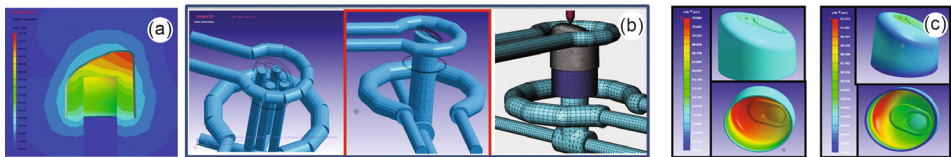
**Figure 1.27** New concepts in product development of injection molding processes

The best opportunities for using CAE in the injection molding process are:

1. At the product design stage and before mold construction: Predict and amend possible defects in product design and reduce the cost for mold opening.
2. After mold construction but before mass production: If the product is defective, but the causes are difficult to solve via onsite mold tests, this can be analyzed to determine the causes for defect generation through regenerating the actual defects and issues via simulation.
3. After mold construction and during mass production: Find out any possibility for yield improvement and molding cycle time shortening via simulation to further increase the productivity.
4. Create an in-house database: Summarize the problem-solving knowledge and create problem-determination SOPs (standard operation procedures) by constantly accumulating project counts.

Hereunder is an example of a cap for spraying deodorant in mass production. How do we utilize CAE to help the manufacture? This situation meets the above-mentioned CAE application opportunity item 3. For the product in mass production, using trial-and-error to further improve productivity or yield is time- and labor-consuming, which makes CAE a pretty good choice in this application.

As shown in Figure 1.28(a), with CAE analysis we can see that the temperature difference between inside and outside of the cap is  $45^{\circ}\text{C}$  in EOC (end of cooling), which leads to thermal stress and causes quality issues. The high product temperature also affects the ejection time (problem discovery).



**Figure 1.28** CAE example: spray deodorant cap

As shown in Figure 1.28(b), originally, the cooling channel design was a big pipe; however, by considering abnormal cooling channel design and comparing three different models, the one in the middle shows the best result. This is a good example of using CAE to save time and labor without redesigning the mold.

As shown in Figure 1.28(c), the new design reduces the temperature difference by  $15^{\circ}\text{C}$ .



Final result: The productivity is increased by 25% as the cycle time is shortened. For an annual production of 4 million pieces, 4 million seconds (46 days) are saved therefrom. In addition, the quality is improved simultaneously as the temperature difference is reduced.

This example clearly tells us that, with proper use of CAE tools, we can improve existing processes without affecting current production lines and with only little cost.

The following chapters will introduce the principles, models, and usage of CAE in detail, from theory to practice, as well as its applications in various industries and molding technologies, so that readers can better understand and learn how to use CAE to solve problems.



# 2

## Material Properties of Plastics

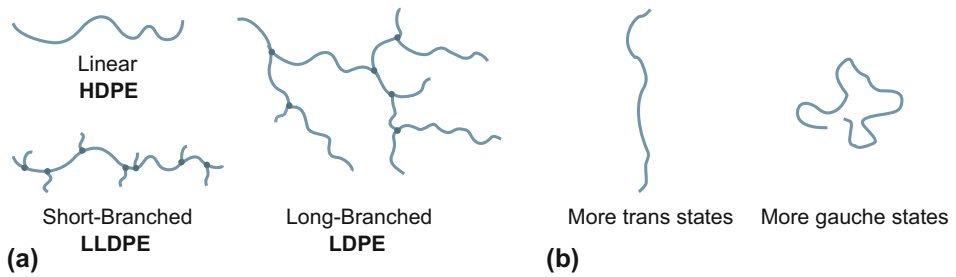
Chen-Chieh (Jye) Wang

Generally, the plastic material for injection molding is in a pellet form, which is heated and melted during the molding process, and is given shape and function before cooling down to become solid again. Therefore, an understanding of different materials regarding their rheological, thermal, thermodynamic, kinetic, chemical, and mechanical properties is essential to obtain the desired application characteristics, functions, molding parameters, product quality, and precision of CAE simulation. Material properties are explored individually in the following sections.

### ■ 2.1 Overview

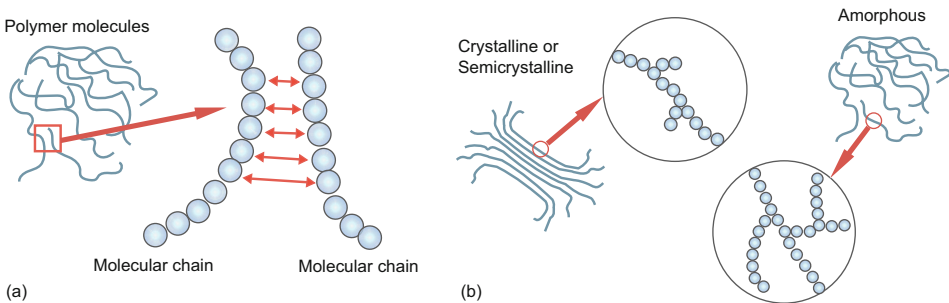
Polymer materials are everywhere, from our daily lives to high-tech fields (such as electro-optical, biomedical, and high performance applications). Polymers consist of many chemical units (monomers) after polymerization, such as polyethylene (PE), whose monomer is ethylene. Polymers have tremendous molecular weights (MW) ranging from tens of thousands to millions and thus are called “macromolecules”.

Figure 2.1(a) shows that the bonding of monomers can be linear or branched. For example, in branched PE, the molecules cannot pack closely together due to steric hindrance of the branches, and so its density is lower; it is therefore called low-density polyethylene (LDPE). In contrast, linear PE is more regular and the polymer chains can pack together more closely and crystallize efficiently; it is therefore called high-density polyethylene (HDPE).



**Figure 2.1** (a) Molecular configurations of polyethylene and (b) conformations of polymer chains

In the polymer chain, the atoms are connected by covalent bonding forces. The bond energy of the C-C covalent bond is around 80 kcal/mol. The rotation of a single covalent bond gives rise to the bond “conformation”, i.e., cis, trans, and gauche states. Since there are many bonds in a polymer chain, a single polymer chain can have tremendously accessible chain conformations. The different chain conformations have different shapes, a fact which also implies a different volume of occupied space, as shown in Figure 2.1(b). Additionally, intermolecular interaction (van der Waals forces) occurs among molecular chains, inducing atoms to pack more closely together, preventing atoms from chain crossover and leading to chain entanglement, as shown in Figure 2.2(a). The entanglement of chains plays an important role in the viscoelastic behavior of materials.



**Figure 2.2** (a) Interactions among macromolecules and (b) classification of thermoplastic polymers

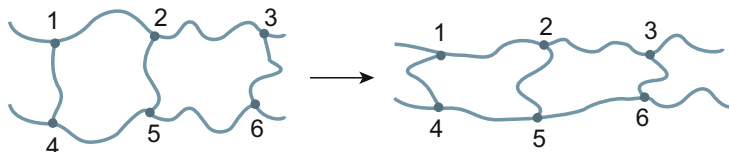
When the polymer material is heated, the thermal energy imparted to the atoms is sufficient to overcome the energy for performing large-scale molecular movements, and the material softens. When the temperature is high enough for the polymer chain to move freely, the material flows like a liquid. A plastic that can be melted by heat and reverts to the solid state after cooling is generally called “thermoplastic”. If the temperature is further increased, the thermal energy may be high

enough to break the covalent bonds. The molecular chain may then break into fragments in a process called “degradation”. In summary, the polymer behaves like a solid when the temperature is lower than the glass transition temperature at which the molecules freeze. The material behaves like a rubber when molecules are able to perform large-scale movements and like a liquid when it can move freely.

In accordance with their molecular morphology in the solid state, thermoplastic polymers can be classified into two categories: crystalline and amorphous. The amorphous morphology has no long-range order structure. In other words, the chains pack randomly throughout the material, e.g. as in PMMA, a-PS, and ABS. In contrast, crystalline polymers (such as i-PP, PE, nylon) can form orderly stacks of folded chains called lamellae, which are like crystals with an orderly arrangement of atoms.

In contrast to thermoplastics, thermoset polymers cure irreversibly. After heating, they cannot return to the original state, which means that they cannot be processed again. Examples are phenolic resins, melamine, UP, PU, and epoxy.

When a thermoset material is heated, its molecular chains will cross-link with each other to form a three-dimensional network structure due to chemical reaction. After the cross-linking reaction, the material cannot flow or be re-formed under the constraint of the cross-linked structure, and exhibits solid behavior, as shown in Figure 2.3. The higher the cross-linking density, the more constrained it becomes and therefore the material becomes harder.



**Figure 2.3** Network structure of thermoset materials

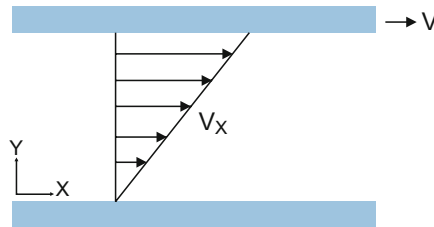
## ■ 2.2 Rheological Properties

The flow behavior of polymers is within the realm of rheology, which is the study of the deformation and flow of materials. Polymer rheology covers experimental research on the measurement of fluid viscosity, the relationship between molecular structure, pressure, and temperature, and the effect on rheological properties of solvents and plasticizers, as well as Newtonian and non-Newtonian fluid mechanics, and other theoretical research such as molecular rheology, which has become

a popular field in recent years. The reason why the rheological behavior of polymeric fluid is different from that of simple molecules is that a polymer's molecular weight is often as high as  $10^5$  to  $10^8$  g/mol, consisting of long-chain molecules, sometimes with branched structure. The rheological behavior of polymers therefore plays an important role in injection molding. When melted plastic is injected into the mold cavity, the flow resistance and behavior are related to its rheological properties with regard to how the mold cavity is filled, how much injection pressure is required to inject the melted plastic through sprues and runners, what the temperatures of the melt and mold should be, etc. It is also instrumental in designing the runner and sprue locations so as to avoid unnecessary packing and weld lines. The shrinkage, warp, and deformation of the product are affected by the molecular orientation, crystallinity, and residual stress after filling and cooling of the melted plastic. In summary, an understanding of rheology is beneficial to product and mold design, which can also help to solve injection molding issues, and derive the greatest benefits from CAE.

### 2.2.1 Viscosity

Consider an incompressible fluid located in the space between two parallel plates, as shown in Figure 2.4.



**Figure 2.4** Flow between two parallel plates

Assume the areas of top and bottom plate are both  $A$ , and the two plates maintain a small distance  $Y$  between each other. If an external force  $F$  is applied to the top plate, the top plate can move at a constant velocity  $V$ , while the bottom plate remains stationary. Such flow is called simple shear flow. It was found by experiment that when a steady state is reached,  $(F/A)$  is in proportion to  $(V/Y)$ , where the proportional constant  $\eta$  denotes the viscosity of the fluid (Equation 2.1).  $(F/A)$  is called the shear stress,  $\tau_{xy}$ , and  $(V/Y)$  is called the shear rate,  $\dot{\gamma}$ , giving Equation 2.2, which is known as Newton's Law of Viscosity:

$$\frac{F}{A} = \eta \frac{V}{Y} \quad (2.1)$$

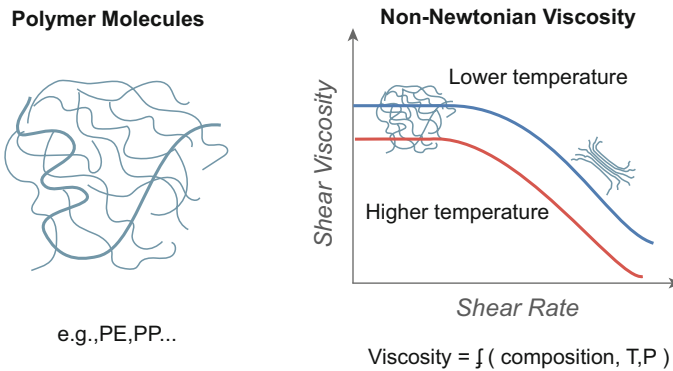
$$\tau_{xy} = \eta \dot{\gamma} \quad (2.2)$$

Shear rate denotes the difference in velocity of each point in the flow field, reflecting the velocity gradient in a flow.

### 2.2.1.1 Effects of Non-Newtonian and Molecular Conformation

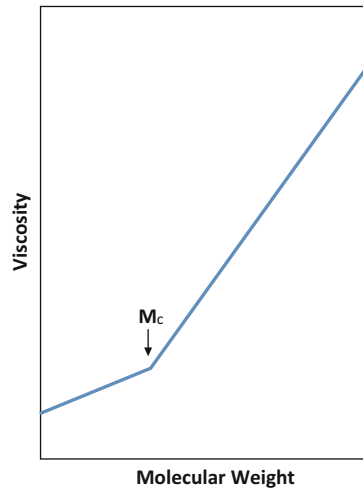
A fluid is defined as being Newtonian only if the stress and shear rate are related by a constant viscosity (Equation 2.2) that does not depend on the stress or shear rate of the flow. The viscosity can be regarded as the resistance to flow and deformation. The resistance results from the collision of and friction among the molecules during flow. It can be influenced by material compositions, temperature, and pressure.

The flow resistance (viscosity) of a polymer depends on the orientation and conformation of molecular chains. Since orientation and conformation vary with the flow fields, the viscosity may change with shear rate, as shown in Figure 2.5.



**Figure 2.5** Molecular structure and viscosity of polymer molecules

For a polymer of low molecular weight, the flow resistance and viscosity are lower because its molecules are shorter, whereas a polymer with longer molecules has a higher viscosity due to the molecular size and the number of entanglements among the molecular chains. The relationship between viscosity and molecular weight is shown in Figure 2.6, where a larger slope is observed once the molecular weight exceeds a critical value, owing to the effect of entanglement.



**Figure 2.6** Viscosity at various molecular weights

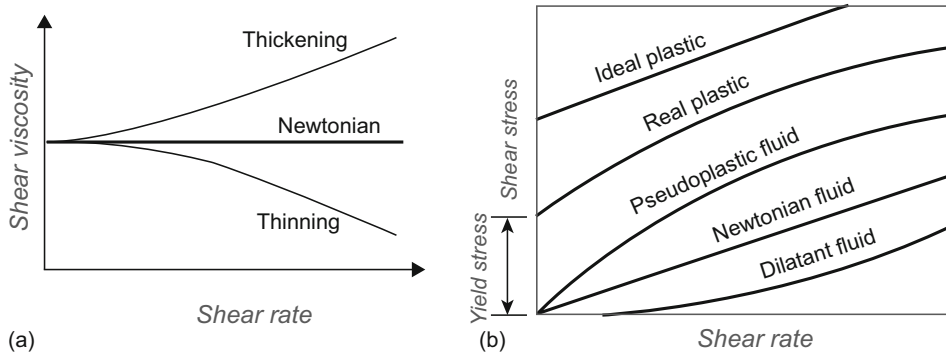
In macromolecules, entanglements act as obstacles to the movement of a polymer chain, creating a restricted tube with surrounding chains in such a way that the chain can only wriggle along the tube, while the lateral motions of the chain are restricted. Such motion is called “reptation”. Based on this model, Doi and Edwards [1] proposed a mathematical derivation that links microscopic molecular topology to macroscopic rheological properties. The results also show that the viscosity increases with about a 3.4 power of the molecular weight [2]. This conclusion is in agreement with experimental measurement for many polymers [3].

### 2.2.1.2 Effects of Shear Rate

Fluids that obey Newton’s Law of Viscosity (Equation 2.2) are called Newtonian fluids, and can be observed in many gases, or liquids and solutions of low molecular weight. Since the viscosity of a Newtonian fluid is irrelevant to shear rate at a constant temperature, the graph showing the relationship between them is just a horizontal line (Figure 2.7(a)). There is a linear relationship between shear stress and shear rate which takes the form of a straight line passing through the origin on the graph (Figure 2.7(b)).

For polymeric fluids, the viscosity usually exhibits shear-rate-dependent properties. A fluid whose viscosity decreases with increase in shear rate (Figure 2.7(a)) is called a shear thinning fluid or pseudoplastic fluid. In contrast, a fluid whose viscosity increases with increase in shear rate is called a dilatant fluid, also known as a shear-thickening fluid.

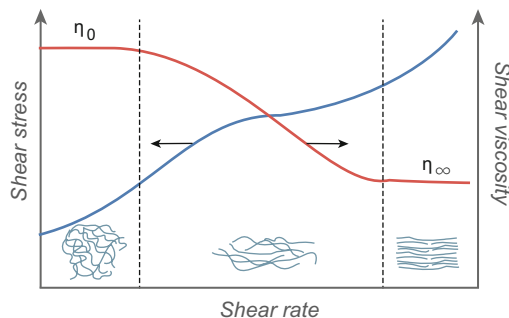




**Figure 2.7** (a) Shear viscosity vs. shear rate and (b) shear stress vs. shear rate

Some fluids, such as suspensions or slurry solutions, usually do not flow under small shear stress. The flow starts when the external force is larger than the yield stress; such a fluid is called a viscoplastic fluid, also known as a Bingham fluid.

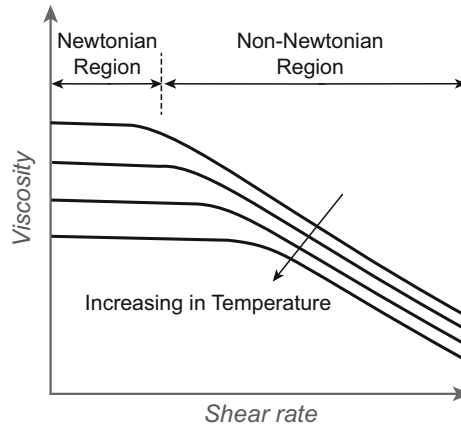
Most polymeric fluids can be classified as pseudoplastic fluids. Figure 2.8 shows the dependence of shear rate on shear stress and viscosity for a typical polymeric fluid under shear flow. With increase in shear rate, the polymer chains start to disentangle and align along the direction of flow. The alignment reduces the molecular interactions, as a result of which the viscosity continues decreasing as the shear rate increases, i.e. shear-thinning behavior occurs. When the shear rate gets extremely high, the oriented molecules do not have sufficient time to revert to the coiled state and are completely aligned under the shear stress of the fluid. The flow resistance and viscosity reach the minimum ( $\eta_{\infty}$ ) theoretically. However, this phenomenon is usually difficult to measure in polymer melts, because the degradation will be very acute under such high shear rates and stress.



**Figure 2.8** Shear viscosity and shear stress vs. shear rate

### 2.2.1.3 Effects of Temperature

The viscosity of polymeric fluids not only is sensitive to the shear rate, but also changes with temperature. This phenomenon of viscosity changing with temperature is also observed in common Newtonian fluids. As shown in Figure 2.9, the curve of viscosity moves toward the bottom left of the graph as the temperature rises. At higher temperatures, the polymer chains have a larger free volume and mobility and so find it much easier to overcome the interaction energy of molecules. Therefore, raising the processing temperature is commonly used to increase the flowability of polymer melts.



**Figure 2.9** Shear viscosity of various temperatures

To describe the temperature effect on viscosity, the shift factor,  $a_T$  is defined as:

$$a_T \equiv \frac{\eta_0(T)}{\eta_0(T_0)} \quad (2.3)$$

where  $\eta_0$  is the zero shear rate viscosity under temperature  $T$  and  $T_0$ , respectively.

The viscosity under various temperatures and shear rates can be expressed as the viscosity at reference temperature:

$$\eta(T, \dot{\gamma}) = a_T \eta(T_0, \dot{\gamma} \cdot a_T) \quad (2.4)$$

Commonly, there are two models to describe the relationship between  $a_T$  and temperature:

1. Arrhenius-type equation:

$$a_T = \exp \left( \frac{\Delta H}{R} \left( \frac{1}{T} - \frac{1}{T_0} \right) \right) \quad (2.5)$$

# Index

## A

advanced hot runner (AHR) 389  
air trap 13, 219, 339  
amorphous 25, 49, 53, 54, 321, 324  
anisotropic 512, 523, 536  
anisotropic rotary diffusion (ARD) model 352  
anisotropic rotary diffusion (ARD) tensor 356  
anisotropic tensor 501  
Arrhenius equation 61  
aspect ratio 353, 359  
autocatalytic kinetic model 67  
Avrami equation 64

## B

back pressure 111, 120, 123, 124, 126  
baffle 289  
ball grid array (BGA) 553  
barrel 6, 7  
bi-injection molding 413, 415  
bilaminate 577  
Bingham fluid 29  
black line 505  
blow-through 442  
boss 79, 82–84, 88  
boundary layer mesh (BLM) 187  
breakthrough 416, 420  
brown part 497  
bubbler 289  
burn mark 13

## C

carbon fiber 539  
Carreau-Yasuda model 32, 33  
cashew gate 95, 253  
Castro-Macosko model 69  
cell growth model 464  
cell nucleation model 465  
ceramic injection molding (CIM) 495  
chamfer angle 73, 78  
chemical foaming 457, 458, 480  
chemorheology model 69  
chip packaging 550  
chip-substrate packaging 552  
chisel gate 252  
co-injection molding 412, 417  
compounding 496  
computational fluid dynamics (CFD) 279, 300  
conformal cooling 293, 299  
continuity equation 174  
continuum surface force 560  
control volume 174  
convected Jeffrey model 38  
conversion 529, 535  
coolant 280, 286, 289, 291, 293, 298  
coolant flow rate 141  
cooling efficiency 291, 299  
cooling stage 105, 116, 140  
cooling temperature 120  
cooling time 73, 115, 120, 135, 140, 294  
Couette flow 501  
cross-link 25, 66  
crystalline 25, 48, 52–54, 321, 324

crystallinity 26, 64  
curing 66, 68, 69  
curing degree 561  
curvilinear flow 501

## D

Darcy's law 523  
defects 1, 10, 13, 17, 18, 20  
degree of cure 69  
delamination 14  
design for manufacture (DFM) 158  
design of experiment (DOE) 332  
diaphragm gate 250  
die swell 36  
differential scanning calorimetry (DSC) 47  
dilatant fluid 28, 32  
disk gate 250  
distinct interface 411, 416  
draft angle 79, 81, 84, 85, 88–90  
dry spot 520  
Dual In-line Package (DIP) 553

## E

edge effect 521, 531  
edge gate 96, 248, 381  
ejection temperature 110, 296  
ejector 95, 102  
elastic modulus 38, 61  
elastic recoil 37  
energy equation 175  
equation of state 49  
extrudate swell 36

## F

fan gate 95, 249  
fan-in 552  
fan-out 552  
feed 106, 125  
fiber 318, 322  
fiber orientation 95, 348, 351, 352, 358, 362

fiber-reinforced polymer (FRP) 512  
fillet 78  
filling stage 105, 114, 132, 136, 138  
filling time 129, 135, 198  
film gate 250  
fingering effect 444, 453  
finite difference method (FDM) 175  
finite element method (FEM) 180  
finite volume method (FVM) 178  
fish eye 14  
flash 11, 12, 110, 202, 211  
flatness 160  
flip chip bonding 551  
flow balance 239, 258, 262, 382  
flow consistency index 32  
flow imbalance 258, 262, 265, 271, 388, 394, 420  
flow length 76, 77, 220  
flow length/wall thickness ratio 76, 160, 219  
flow mark 14, 203  
flow rate 200, 232  
fluid-assisted injection molding 438  
fluid-structure interaction (FSI) 563, 569, 571, 574  
foaming with counter pressure 462  
Folgar-Tucker diffusion model 354  
fountain 193  
fountain flow 416  
frame level packaging 553  
frozen layer 194, 219  
full shot overflow method 437  
full shot pushback method 438

## G

gas-assisted injection molding (GAIM) 433  
gate sealing 256  
Giesekus model 39  
glass transition 31, 46, 49, 50, 54, 60  
glassy region 60  
granulation 496

**H**

heat capacity 46, 47  
heat flux 56  
heating coil 384, 388, 391, 393  
hesitation 15, 16, 219  
hesitation mark 442  
holding stage 107, 109  
hollowed core ratio 434, 445  
hopper 3, 6, 10  
hot runner system 379, 389  
hot spot 297  
hot-tip gate 381  
hybrid mesh 266

**I**

impregnation 514, 520, 544  
improved ARD and retarding principal  
rate (iARD-RPR) model 352, 358, 361  
injection pressure 112, 132–136  
injection velocity 129  
insert molding 411  
integrated circuit (IC) 549  
isotropic 535  
isotropic rotary diffusion 352, 354

**J**

Jeffery's hydrodynamic model 352  
jetting 16, 91, 94, 202, 246, 249

**K**

knock-out pin gate 252

**L**

laminar flow 291  
Land Grid Array (LGA) 553  
lapped gate 249  
lay-up 516, 522, 534  
lead frame 550, 558, 563  
liquid composite molding (LCM) 513  
long fiber reinforced thermoplastic (LFRT)  
348

**M**

manifold 382, 388  
mat 514  
Maxwell model 38, 61  
melt fracture 37, 202  
melt front area (MFA) 200  
melting core 258  
melt temperature 110  
metal insert 332, 335  
metering stroke 111, 126  
MFR (melt flow rate) 110  
microcellular foam 458, 480  
modified Cross model 32  
modified Tait model 52  
modified White-Metzner model 39  
mold clamping 105, 106  
mold design 89  
molded underfill (MUF) 563  
molding cycle 105, 110, 135  
molding instability 167  
molding stability 167  
molding window 110  
mold temperature 110, 141  
momentum equation 175  
multi-cavity system 260, 262  
multi-component molding (MCM) 411,  
417  
multi-die stacking 569

**N**

Newtonian fluid 30, 32, 38  
non-Newtonian fluid 25  
nozzle 105, 106, 112, 114, 122, 125, 127  
nozzle tip 381

**O**

ON/OFF control 385  
over-molding 411

**P**

package-in-package (PiP) 569  
packing pressure 107, 112, 115, 120

packing stage 105, 115, 136, 138  
 packing time 120, 139  
 paddle shift 562, 574  
 particle volume fraction 500  
 permeability 523, 540  
 Phan-Tien and Tanner (PTT) model 40  
 PID control 386  
 pin gate 95, 251  
 Pin Grid Array (PGA) 553  
 pin movement control 404  
 pin through hole 552  
 plasticizing stage 105, 111, 113  
 porosity 524, 528  
 powder injection molding (PIM) 495  
 preform 517, 525, 539  
 Pressure-Volume-Temperature-Cure (PVTC) model 563  
 Pressure-Volume-Temperature (PVT) 318, 324, 332  
 primary fluid penetration 435  
 process condition 111, 120

## Q

Quad Flat No-leads (QFN) 553

## R

race-track 161, 219  
 reduced strain closure (RSC) model 352, 357  
 reflow soldering 553  
 relaxation modulus 61, 67, 562  
 relaxation time 38, 39, 67  
 reptation 28  
 Reynolds number 101, 291, 300  
 rib 79, 80, 83, 84  
 ring gate 250

## S

screw 3, 6–8, 14  
 secondary penetration 453  
 Seemann composites resin infusion molding process (SCRIMP) 518

sequential multiple-shot molding 411  
 shape factor 353, 359  
 shark skin 37  
 shear layer 194  
 shear rate 26–28, 30–33, 39, 68, 258, 265  
 shear stress 26, 28, 37, 65  
 shear-thinning 196  
 shelf level packaging 553  
 short fiber reinforced thermoplastic (SFRT) 348  
 short shot 10, 202, 218  
 side gate 248  
 sink mark 12, 79, 83, 441  
 solder bump 551  
 specific volume 50, 51  
 Spencer-Gilmore-C model 53  
 Spencer-Gilmore model 52  
 splays 16, 17  
 spoke gate 251  
 sprue gate 96, 247  
 stress mark 15  
 submarine gate 252  
 suck back 123, 125, 126, 132  
 supercritical fluid (SCF) 458  
 surface mounting 552  
 System-in-a-Package (SiP) 554, 569  
 System-on-Chip (SoC) 554

## T

Tait model 52  
 tape-automated bonding 550, 554  
 thermal conductivity 56  
 thermal pin 290  
 thermal sprue gate 381  
 thermoplastics 25, 51  
 thermoset 25, 66, 69  
 Thin Small Outline Package (TSOP) 553  
 transfer molding 554  
 tubeless siphon 36  
 tunnel gate 95, 252  
 turbulent flow 291

**U**

U-curve theory 199  
underfill 554, 560  
upper convected Maxwell model 38

**V**

vacuum-assisted resin transfer molding (VARTM) 518  
valve gate 96, 253, 381, 404  
venting 83, 102  
viscoelastic flow 39  
viscoelastic fluid 35, 61  
viscoelasticity 60  
viscosity 26, 28, 30–33, 38, 39, 66, 68, 69  
void 12, 80  
void trapping 564  
VP switch 136, 138, 209

**W**

wafer-level chip scale packaging (WLCSP) 552  
wall thickness 73, 76, 77, 80, 82, 83, 85, 91  
warp 11  
water-assisted injection molding (WAIM) 433  
wave soldering 553  
welding angle 93  
weld line 17, 91, 244  
White-Metzner model 39  
wire bonding 550, 554  
wire sweep 561  
wire sweep index (WSI) 567  
WLF Equation 31  
woven 514, 528, 530, 535

**Y**

yield stress 33